

# Probing Electric and Magnetic Fields with a Moiré Deflectometer

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## Abstract

A new contact-free approach for measuring simultaneously electric and magnetic field is reported, which considers the use of a low energy ion source, a set of three transmission gratings and a position sensitive detector. Recently tested with antiprotons [1] at the CERN Antiproton Decelerator facility, this paper extends the proof of principle of a moiré deflectometer [2] for distinguishing electric from magnetic fields and opens the route to precision measurements when one is not limited by the ion source intensity. The apparatus presented, whose resolution is mainly limited by the shot noise is able to measure fields as low as  $9 \text{ mV m}^{-1} \text{ Hz}^{-1/2}$  for electric component and  $100 \text{ } \mu\text{G Hz}^{-1/2}$  for the magnetic component. Scaled to 100 nm pitch for the gratings, accessible with current state-of-the-art technology [3], the moiré fieldmeter would be able to measure fields as low as  $22 \text{ } \mu\text{V m}^{-1} \text{ Hz}^{-1/2}$  and  $0.2 \text{ } \mu\text{G Hz}^{-1/2}$ .

*Keywords:* Fieldmeter, Lorentz force, Moiré effect

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## 1. Introduction

Depending on the frequency range considered, electric field meters usually rely on different operating principles. Antennas reach the best performances to measure time-varying electric fields, when frequencies typically overcome 100 kHz. Reference [4] gives the example of a dipolar double probe, able to measure electric fields with a sensitivity of  $E_{\text{min}} = 1 \text{ mV m}^{-1}$  at several MHz. Instead, the highest sensitivities for static or low-frequency electric fields are achieved with “voltmeter-type” sensors where the potential difference between two plates placed apart is precisely measured. Krupka et al. [5] reports for instance a sensitivity of  $2 \text{ } \mu\text{V m}^{-1} \text{ Hz}^{-1/2}$  at 100 Hz with plates placed 33 cm apart. Although those devices show a high sensitivity, the field magnitude is indirectly evaluated by the amount of charges it induces.

Another category of apparatus builds on free charges in vacuum. The use of particle beams, combined with a position sensitive detector, allows to perform precise contact-free measurements

over large experimental volumes and to probe directly the field itself. The steered electron field sensor [6], in which two anodes measures the shift induced by an external electric field on an electron beam, is for example able to resolve a field of  $34 \text{ mV m}^{-1} \text{ Hz}^{-1/2}$  at 10 Hz. In its current state, such a device is however not able to determine if the shift measured is due to an electric or a magnetic field. A similar approach is here reported, which presents the advantage of distinguishing the electric from the magnetic field component with the same device.

## 2. Moiré Fieldmeter

### 2.1. Moiré principle

The principle of the moiré fieldmeter can be seen as an extension of the simple setup depicted in figure 1(a) In this configuration, a non-collimated beam passes through two apertures separated by a distance  $L$ , which constrain the trajectories of the particles reaching the detector. Undelected particles such as neutral atoms conserve straight trajectories throughout the whole apparatus while particles submitted to a force will experience an acceleration in the vertical direction leading to a parabolic trajectory. The shift  $\Delta y$  between the two

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48 impacts on the position sensitive detector is given  
 49 by  $\Delta y = a\tau^2$  where  $a$  is the acceleration in the di-  
 50 rection orthogonal to the slits and  $\tau = L/v_z$  is the  
 51 time of flight between the two slits.

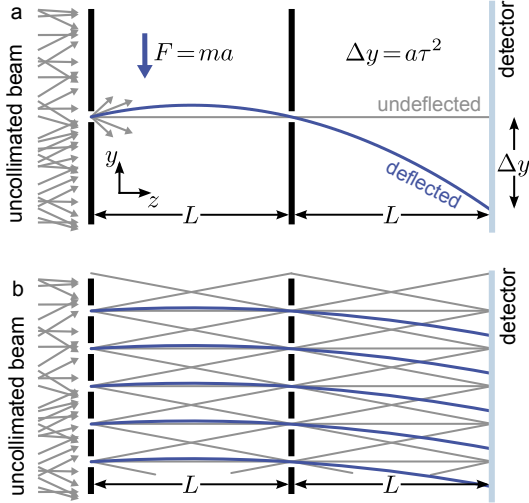


Figure 1: a) Two slits separated by a distance  $L$  restrict the path of a beam to a specific trajectory. b) Replacing the slits by two gratings increases the flux of particles reaching the detector. Since the first grating constrains the ions trajectories, the moiré device does not require the beam to be collimated (image from [7]).

52 If the two slits are replaced by two gratings hav-  
 53 ing a certain periodicity  $d$ , the pattern seen on the  
 54 detector plane becomes a collection of fringes with  
 55 same periodicity as the gratings (figure 1(b)). The  
 56 moiré fieldmeter gives hence a measurement of the  
 57 field, assumed homogeneous, over the whole length  
 58 of the apparatus. It can be particularly beneficial  
 59 for experiments dealing with fields which needs to  
 60 be controlled over large volumes. Observing such a  
 61 pattern can however be problematic if the slits sep-  
 62 aration gets smaller than the detector resolution.  
 63 Adding a third grating with the same periodicity as  
 64 the first two, but tilted by a small angle, allows to  
 65 take advantage of the moiré effect to reveal macro-  
 66 scopic fringes orthogonal to the slit orientation as  
 67 shown in figure 2.

68 For a small angle between the gratings, the  
 69 macroscopic fringes periodicity  $D$  is directly pro-  
 70 portional to the gratings pitch and scales with the  
 71 inverse of the angle  $\alpha$  such that  $D = d/\sin \alpha$ . The  
 72 visibility  $\nu = (I_{\max} - I_{\min})/(I_{\max} + I_{\min})$  of the  
 73 macroscopic pattern formed depends on the open  
 74 fraction of the gratings used. It is equal to 1 for

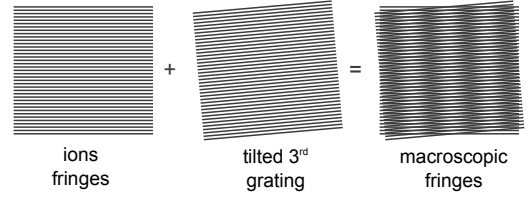


Figure 2: A third tilted grating placed behind the fringes but tilted by a small angle allows one to take advantage of the moiré effect to reveal a macroscopic pattern orthogonal to the slit orientation.

75 open fraction until 25 % and then drops rapidly to  
 76 zero for 50 % open fraction, when the slits is exactly  
 77 half of the grating periodicity. More details about  
 78 the moiré principles can be found in reference [2].

## 79 2.2. Decoupling magnetic and electric components

80 When affected by both an electric and a magnetic  
 81 field, charged particles experience Lorentz forces,  
 82 translating into an acceleration  $a = \frac{q}{m}|\vec{E} + \vec{v} \wedge \vec{B}|$ .  
 83 Following the axis convention of figure 1, and for  
 84 small radial velocities<sup>1</sup>, the field components lead-  
 85 ing to a shift along the  $y$  axis are trivially the com-  
 86 ponents along  $y$  for  $\vec{E}$  and along  $x$  for  $\vec{B}$ . Introduc-  
 87 ing  $V_{\text{acc}}$  the acceleration voltage of the ions (lead-  
 88 ing to an energy  $q \cdot V_{\text{acc}}$ ), the shift due to the Lorentz  
 89 force writes:

$$\Delta y = \frac{L^2}{2V_{\text{acc}}} E_y + \sqrt{\frac{q}{mV_{\text{acc}}}} L^2 B_x. \quad (1)$$

90 The knowledge of  $\Delta y$  for two different accelera-  
 91 tion voltages or two different ion species (with dis-  
 92 tinct charge-to-mass ratios) leads therefore to a sys-  
 93 tem of linear equations with a unique solution in  
 94  $E_y$  and  $B_x$ . Since neutral particles do not experi-  
 95 ence any force when placed in constant electric and  
 96 magnetic fields, they are used to create a reference  
 97 pattern. This extends the measurement of refer-  
 98 ence [1], where only the magnitude of the force is  
 99 measured without probing its nature.

## 100 2.3. Resolution limit

101 The determination of the phase shift between  
 102 the deflected particles and the neutral reference is  
 103 depicted schematically in figure 3. Following the  
 104 mathematical treatment given in reference [7], any

<sup>1</sup>such that  $v_x \cdot B_z$  becomes negligible in comparison with  $v_z \cdot B_x$ .

105 phase shift measured on the detector is limited statistically by the shot-noise leading to an uncertainty  
 106 proportional to  $1/\sqrt{N}$ .  
 107

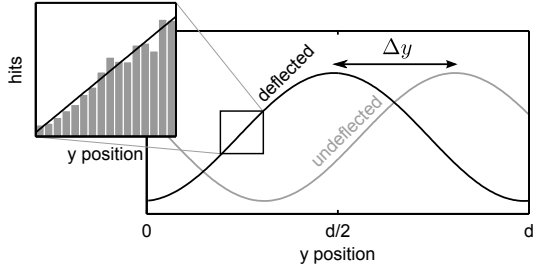


Figure 3: The fringe pattern is shifted by  $\Delta y$  due to a uniform acceleration (image from [7]).

The minimal detectable shift is expressed as:

$$\Delta y_{\min} = \frac{d}{2\pi\nu\sqrt{N}}, \quad (2)$$

108 where  $\nu$  is the fringes visibility,  $d$  the grating peri-  
 109 odicity and  $N$  the number of particles detected. By  
 110 using equation (2), the minimal detectable electric  
 111 field writes:

$$\begin{aligned} E_{\min} &= \frac{dV_{\text{acc}}}{\pi\nu L^2\sqrt{N}}, \\ B_{\min} &= \frac{d}{2\pi\nu L^2\sqrt{N}} \sqrt{\frac{mV_{\text{acc}}}{q}}. \end{aligned} \quad (3)$$

112 For a visibility of 1, a typical ion flux of 0.1 pA  
 113 (corresponding to 10 000 particles detected per second)  
 114 and a 171 mm distance between the gratings, the minimal  
 115 field detectable with 2 keV ions is  $9 \text{ mV m}^{-1} \text{ Hz}^{-1/2}$  and  
 116  $100 \text{ } \mu\text{G Hz}^{-1/2}$  for the magnetic field. For a given  
 117 geometry of the grating, the visibility is also sensitive to  
 118 the velocity distribution of the beam, affecting the resolution  
 119 limit of the fieldmeter. Indeed, in the presence of any force,  
 120 slow particles experience bigger deviations than fast ones.  
 121 As a consequence, the fringes minima and maxima can  
 122 possibly overlap such that the patterns smears out. One  
 123 should notice that the detector resolution affects also the  
 124 fringe visibility through the uncertainty it causes on each  
 125 particle impact's coordinates. Convolving the fringes pattern  
 126 with a gaussian distribution, we estimate the visibility to  
 127 decrease by 20 % for a resolution as high as 10 %  
 128 of the periodicity.  
 129  
 130

#### 2.4. Field corrective factor

131 Because of its metallic parts, the moiré deflectometer  
 132 bends the field lines when placed inside a uniform electric  
 133 field. As a consequence, the field magnitude between the  
 134 gratings gets effectively smaller. The correcting factor  $f$   
 135 accounts for this diminution. From Finite Elements Method  
 136 simulation, we estimate this factor to be of the order of  
 137  $f = 0.87$  for a setup consisting of only three free-standing  
 138 gratings (assuming for instance that the gratings mechanical  
 139 supports are made of a material with small permittivity  
 140 ( $\epsilon_R \simeq 1$ )). A view of the electric field distribution  
 141 around the gratings and its evolution (for the vertical  
 142 component) along a line going through the centre of the  
 143 deflectometer (dashed line) are shown in the figure 4.  
 144 The simulation is done with SIMION 8.0 [8] for an ambient  
 145 field of  $1 \text{ V m}^{-1}$ .  
 146  
 147  
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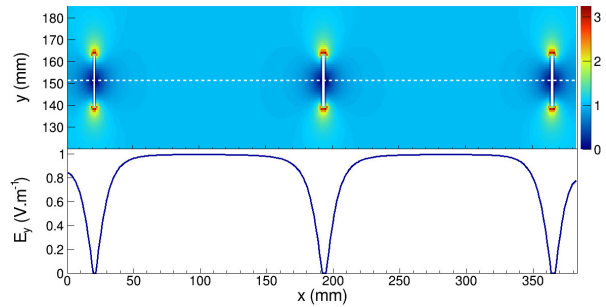


Figure 4: (top) Electric field distribution simulated with SIMION 8.0 [8] for an ambient field of  $1 \text{ V m}^{-1}$ . The field magnitude gets higher around the gratings edges. (bottom) Profile of the vertical component of the field along the axis of the deflectometer (white dashed line on the top picture).

#### 2.5. Maximal operating frequency

149 Assuming a readout fast enough for the imaging  
 150 detector, the moiré fieldmeter is in principle not limited  
 151 to static fields. In our setup, the maximal operating  
 152 frequency is however imposed by the time of flight of the  
 153 protons along the deflectometer. For 2 keV protons and  
 154  $L = 171 \text{ mm}$ , the time of flight between the first and  
 155 the third grating is  $\Delta t = 276 \text{ ns}$ , corresponding to a  
 156 maximal frequency of 1.8 MHz.  
 157  
 158

### 3. Experimental Implementation

#### 3.1. Setup

A schematic view of the system is shown in figure 5. The beam is exiting an Electron Cyclotron Resonance (ECR) ion source able to produce protons,  $H_2^+$  and  $H_3^+$  ions distinguished by the use of a Wien Filter. Its energy can be tuned from 500 eV to 2 keV and the intensity delivered ranges from few nA to less than 1 pA. The energy spread of the beam measured at the entrance of the fieldmeter is typically of the order of 1 to 2 %. More details on the source can be found in reference [9]. A nitrogen gas target placed right behind the source allows one to select either ions or hydrogen atoms formed by electron capture by tuning the pressure from  $10^{-9}$  to  $10^{-3}$  mbar.

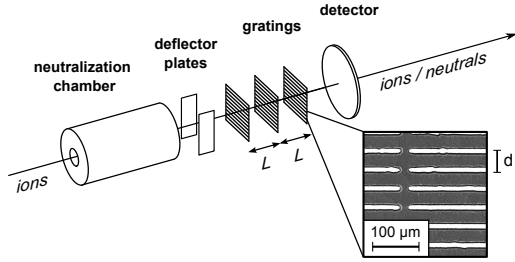


Figure 5: Schematic view of the experimental setup. The ions are sent through three transmission gratings and reach an imaging detector. For referencing purposes, a gas target and a set of deflector plates placed downstream enables one to switch from ion beam to neutral beam. The close-up shows a Scanning Electron Microscopy picture of the gratings.

By doing so, one benefits from an inline neutral beam for calibrating the fieldmeter. A set of two electrostatic deflector plates is used to eliminate the eventual remaining ions when neutral particles are selected. The beam is sent through three metal-coated silicon gratings with  $40 \mu\text{m}$  periodicity with an open fraction of the order of 20 %, and spaced by a distance which may be tuned between 34 mm and 171 mm. Each grating is  $10 \times 10 \text{ mm}^2$  with a thickness of  $100 \mu\text{m}$  and is mounted on vacuum compatible piezo actuators, allowing rotation (with millidegree resolution) around the beam axis for the two first ones. To avoid the slits to collapse on themselves, support structures are added to the gratings during the etching process. They consist in structures oriented perpendicularly to the slits and with periodicity ranging from one to several millimeters

depending on each grating. Finally, a 25 mm in diameter Micro Channel Plate (MCP) with  $12 \mu\text{m}$  channel size stacked to a resistive anode detects the particles outcoming the gratings.

#### 3.2. Pattern reconstruction

The two-stages MCP amplifies the signal for each hit with a typical gain around  $2 \cdot 10^6$ . The Quantar Technology 3390A Resistive Anode Encoder [11] (RAE) converts then the analog signals to a set of digital coordinates stored in a  $256 \times 256$  pixels matrix. The spatial resolution of this model is of the order of  $250 \mu\text{m}$  with typical background count rate of 5 per second [11]. For each ions species considered, the images are acquired with a flux of approximately 1 kHz during 1 min such than  $10^4$  to  $10^5$  events are taken into account in average. To minimize the effect of the non-uniformity of the detector (dead and hot stripes), the RAE is rotated with respect to the expected fringes orientation. Figure 6 shows a typical image of the moiré fringes, with a visibility of 0.92, obtained with neutral hydrogen.

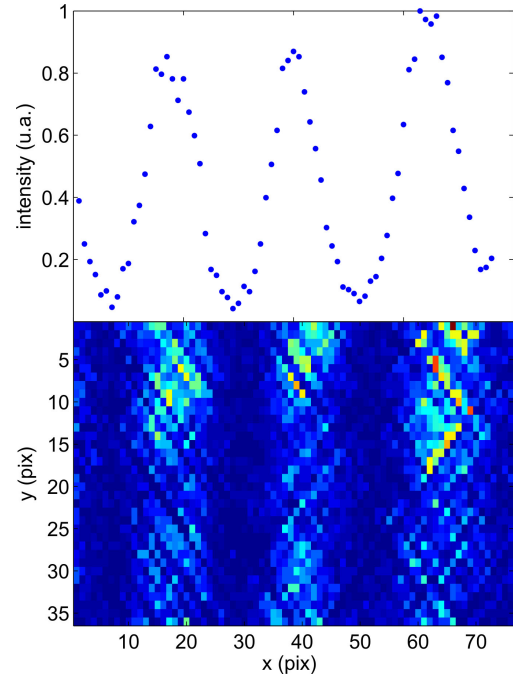


Figure 6: View of the moiré fringes obtained with neutral hydrogen on the resistive anode detector. The upper part plot represents the projection with a high visibility of 0.92. Such a pattern is used as a reference for measuring the shift difference between the ions.

213 *3.3. Phase difference measurement*

214 The pattern formed is then fitted by the function<sup>2</sup>

$$I(y) = \frac{a_0}{2} + \sum_{n=1}^{+\infty} a_n \cos\left(\frac{2\pi n}{d}(y + \phi)\right), \quad (4)$$

where the  $a_n$  coefficients are given by:

$$a_n = 4\eta^3 \text{sinc}^3(\pi\eta n) \cos(\pi\eta n) \quad \forall n \in \mathbb{N}, \quad (5)$$

215 standing for the convolution of the last grating's  
 216 transmission function with the projection of the sec-  
 217 ond grating's pattern with open fraction  $\eta$ . As the  
 218 Fourier coefficients get rapidly negligible [12], only  
 219 the first ones (until  $n \leq 2$ ) are taken into account  
 220 in the fit.

221 The field measurement is performed inside a  
 222 three layers mu-metal magnetic shield with a shield-  
 223 ing factor around 1000. The shield, also operat-  
 224 ing as a Faraday cage, guarantees a magnetic field  
 225 below 20 mG and  $10 \text{ V m}^{-1}$  for the electric field.  
 226 The moiré patterns for neutral hydrogen, protons,  
 227  $H_2^+$  and  $H_3^+$  ions at 2000 eV and for a distance of  
 228 171 mm between the gratings are plotted in figure 7.  
 229 Although the total number of particles detected for  
 230 each pattern is of the order of  $10^4$ , fluctuations due  
 231 to the RAE response can still be seen on the profiles.  
 232 The corresponding shifts, scaled down to the origi-  
 233 nal  $40 \mu\text{m}$  periodicity of the gratings, are listed in  
 234 table 1. The fit uncertainties originate from the non  
 235 uniformity of the detector response and the  $2.3 \mu\text{m}$   
 236 error on the pattern periodicity.

	shift $\Delta y$ ( $\mu\text{m}$ )	error ( $\mu\text{m}$ )
protons	1.98	0.37
$H_2^+$	1.35	0.26
$H_3^+$	1.14	0.23

Table 1: Measured shift of the fringe pattern for  $H_3^+$ ,  $H_2^+$  ions and protons.

237 Considering each combinations of ion species  
 238 (proton with  $H_2^+$ , proton with  $H_3^+$  and  $H_2^+$  with  
 239  $H_3^+$ ) leads to three distinct measurements for the  
 240 electric and magnetic fields following the equation  
 241 system (1). Taking their mean values leads to:

$$\begin{aligned} E &= 0.91 \pm 0.31 \text{ V m}^{-1} \\ B &= -15.2 \pm 6.8 \text{ mG} \end{aligned} \quad (6)$$

<sup>2</sup>The detailed mathematical treatment to obtain the Fourier decomposition can be found in reference [12].

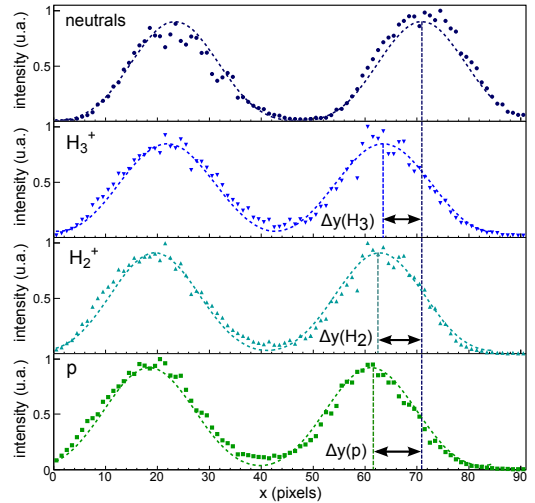


Figure 7: Moiré patterns for (from top to bottom) hydrogen,  $H_3^+$ ,  $H_2^+$  ions and protons. One can notice the spatial shift between the three species, listed in table 1. Measuring those shifts enables one to evaluate the magnitude of the fields acting on the ions.

242 where the errors originate from the standard de-  
 243 viation of the different combinations.

244 *3.4. Test of the fieldmeter*

245 The reliability of the fieldmeter is now evaluated  
 246 with an homogeneous and known magnetic field.  
 247 To do so, the three gratings, spaced here by 34 mm,  
 248 are placed between two large rectangular Helmholtz  
 249 coils with dimensions  $500 \times 280 \text{ mm}$ , ensuring a  
 250 uniform magnetic field (within 1 % based on Biot-  
 251 Savart calculation [13]) between the gratings. As  
 252 the distance between the gratings is strongly re-  
 253 duced to guarantee the magnetic field homogeneity,  
 254 the sensitivity of the apparatus decreases quadra-  
 255 tically to  $2.4 \text{ mG Hz}^{-1/2}$ . A reference picture of  
 256 the fringes is taken with neutral particles and for  
 257 each current value, the shift  $\Delta y$  for 2 keV protons,  
 258  $H_2^+$  and  $H_3^+$  ions are obtained as in the previous  
 259 section. The  $x$ -component of the magnetic field is  
 260 independently measured with a Hall probe placed  
 261 in the vicinity of the gratings.

262 The evolution of the magnetic and electric fields  
 263 measured by the moiré fieldmeter as a function of  
 264 the coil current  $I$  is given in figure 8. An affine  
 265 function with a slope of  $2.97 \text{ G/A}$  is fitted to the  
 266 data and compared to the Hall probe output  
 267 ( $3.01 \pm 0.07 \text{ G/A}$ ). Although the slopes are com-  
 268 patible, a 410 mG offset is measured between the

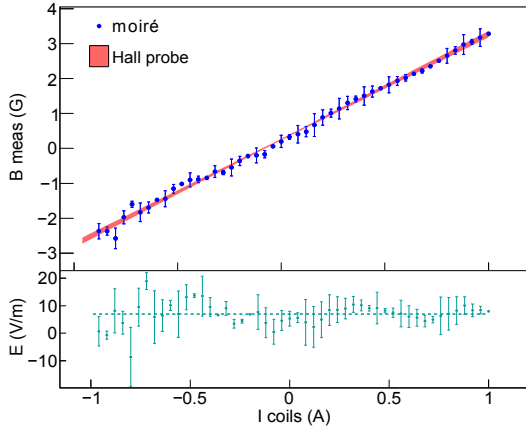


Figure 8: Measured electric and magnetic fields as a function of the coils current. The magnetic field, evaluated separately by a Hall probe, shows a linear dependency while the electric field remains constant of the order of  $6.96 \text{ V m}^{-1}$ . On the upper plot, an offset field of 410 mG is added to the Hall probe response.

two devices. The difference is imputed to the improper nulling of the Hall sensor, while the moiré is calibrated “in absolute” by the neutrals and at the position of interest (in situ). One can notice on the other hand the stability of the electric field with the coil current.

## 4. Discussion

### 4.1. Charge-up effects

The strength of the moiré deflectometer as a fieldmeter relies on the fact that it does not create its own field. For this reason, every metallic part is grounded and the gratings, made of silicon, are metalized by an alloy of gold and palladium. The stability of the coating has been tested under the SEM microscope after one week of irradiation. For the intensity of ions considered (at most at the level of  $I = 1 \text{ pA}$ ), the stray resistance between the gratings and their support, of the order of a few ohms, can be responsible of an electric field at worst at the level of  $R \cdot I/d \simeq \mu\text{V m}^{-1} \text{ Hz}^{-1/2}$ , negligible for the sensitivity achieved. Reference [14] gives a picture illustrating how a local potential, a wire kept at a few volts, distorts Talbot-Lau Electron fringes.

### 4.2. Ions monochromaticity and visibility drop

For the energy spread considered, one can calculate the field leading to an overlap of the patterns created by the fastest and slowest ions. The

worst case being when the two populations presents a phase shift of half a period, leading to a zero visibility. For a given energy spread  $\Delta V_{\text{acc}}$ , the patterns generated by slow and fast particles are separated by  $d/2$  when the critical electric field  $E_c$  is applied, such that:

$$\begin{cases} \Delta y = \frac{L^2}{2V_{\text{acc}}} E_c \\ \Delta y + \frac{d}{2} = \frac{L^2}{2(V_{\text{acc}} + \Delta V_{\text{acc}})} E_c. \end{cases} \quad (7)$$

Solving this equation system allows one to retrieve the expression of the critical fields, which defines the robustness of the moiré fieldmeter. These equations can be translated into the following expressions for the critical magnetic and electric fields:

$$\begin{aligned} E_c &= \frac{dV_{\text{acc}}^2}{L^2 \Delta V_{\text{acc}}}, \\ B_c &= \frac{d}{L^2} \sqrt{\frac{m}{q}} \frac{V_{\text{acc}}^{3/2}}{\Delta V_{\text{acc}}}. \end{aligned} \quad (8)$$

For a 2 keV proton beam with 1 % energy spread and  $L = 171 \text{ mm}$ , it corresponds to  $E_c = 273 \text{ V m}^{-1}$  and  $B_c = 6.3 \text{ G}$ .

### 4.3. Absolute measurement and phase shift uncertainty

As any phase difference is measured modulo  $2\pi$ , the phase shift considered between the two patterns is subject to an ambiguity (there is no way to distinguish a certain shift from the same shift modulo the pattern’s period). It defines therefore the range of the field that can be measured by the moiré fieldmeter, dependent on the grating periodicity. From equation (1), this is expressed as:

$$\begin{aligned} \Delta E_y &= \frac{2dV_{\text{acc}}}{L^2}, \\ \Delta B_x &= \frac{d}{L^2} \sqrt{\frac{mV_{\text{acc}}}{q}}. \end{aligned} \quad (9)$$

For 2 keV ions and a pitch of  $d = 40 \text{ }\mu\text{m}$ , it corresponds to  $5.5 \text{ V m}^{-1}$  and  $63 \text{ mG}$  for  $L = 171 \text{ mm}$  ( $35 \text{ V m}^{-1}$  and  $1.6 \text{ G}$  for  $L = 34 \text{ mm}$ ). In practice, the moiré fieldmeter is therefore a fine measurement device which needs to be associated to a standard field meter giving the order of magnitude.



## 5. Conclusion

A new method for measuring simultaneously electric and magnetic fields has been presented. A sensitivity of  $9 \text{ mV m}^{-1} \text{ Hz}^{-1/2}$  and  $100 \text{ }\mu\text{G Hz}^{-1/2}$  has been achieved with a low-energy ion source delivering typically  $10^7$  particles per second, a set of three transmission gratings with  $40 \text{ }\mu\text{m}$  periodicity and a resistive anode detector. The monochromaticity of the ion source allows the device to measure fields until  $E_c = 273 \text{ V m}^{-1}$  and  $B_c = 6.3 \text{ G}$ . Higher performances can be in principle achieved with gratings having sub-micron pitches. For  $100 \text{ nm}$  periodicity transmission gratings as the one used in reference [3], the moiré fieldmeter would be able to measure fields as low as  $22 \text{ }\mu\text{V m}^{-1} \text{ Hz}^{-1/2}$  and  $0.2 \text{ }\mu\text{G Hz}^{-1/2}$  under the same conditions.

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